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UNITED STATES PATENT APPLICATION

of

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and

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for

RADIATION DETECTOR

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[0001]

BACKGROUND OF THE INVENTION

[0002] The apparatus being provided relates to the field of engineering physics, in particular, to the radiation detecting technique and may be used for photometry, dosimetry and also for measurements of the space-energy characteristics of optical and ionizing-radiation fields. The radiation detector used in optical radiation detection and photometry application is known [1]. The detector comprises a photodiode placed either in parallel with a load or connected in series with a bias voltage source and with a load in the simplified case [1]. A current or charge-amplifier input circuit is conventionally used therein as a load. One-dimensional and two-dimensional photodiode and phototransistor arrays [2,3], as well as image detectors based on the charge-coupled devices (CCD) [4] are also known. Said devices detect space-energy characteristics of optical radiation fields. The ionizing radiation detectors used for detection dosimetry and spectrometry of nuclear radiation are known [5]. The construction of said detectors is similar to that of optical radiation detectors, in which ionization chambers, proportional counters, semiconductor sensors, scintillation counters or photodiodes paired with scintillators are used instead photodiodes [5]. Ionizing-radiation coordinate-sensitive detectors (IRCSD) for making one-dimensional and two-dimensional coordinate analysis are known and used in the nuclear experiment techniques for detecting elementary particle traces and

measuring a spatial distribution of a nuclear particle flow [6,7]. Said detectors make up either a system of wire electrodes disposed in a common gas volume or a system of strip electrodes sputtered on a silicon crystal surface and coupled with the electronics for reading the coordinate information.

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[0003] Of conventional radiation detectors, the detector described in [1] is most similar to the detector being provided by the engineering nature thereof. Said detector comprises a photodiode, placed in parallel with the load or connected in series with the load or the bias-voltage source. In this case, the dc current or charge-amplifier input circuit serves as the load. Said detector is intended to detect an optical radiation and may be used to detect an ionizing radiation by coupling the photodiode with a scintillator. A low sensitivity resulting from the noises and zero drift of the dc amplifier used as the detector load is a disadvantage of said detector.

[0004] The subject-matter of the first embodiment of the invention being claimed is that in the radiation detector comprising a series-connected photodiode and a load, with the load being coupled with the photodiode through a signal contact and at the other side being connected to a common bus; a transistor and an interrogation pulse generator are additionally incorporated, with the second photodiode electrode being coupled with the first electrode of the transistor, a control electrode

of which is coupled with the interrogation pulse generator output, and the third transistor electrode is coupled with the common bus. In addition, N groups of elements, each consisting of the series-connected photodiode and transistor, are placed in parallel with the load, and the interrogation pulse generator comprises N outputs, each being coupled with the transistor control electrode from the respective element groups, where N - integer > 1. Alternatively, the detector may comprise L loads, with the Ni groups of elements being placed in parallel with each i-th load, and the total number of groups of elements in the detector being equal to the number N of outputs of the interrogation pulse generator, where L - an integer >1 and N, - positive integer. Additionally, capacitors are placed in parallel with photodiodes.

[0004] The subject-matter of the second embodiment of the invention being claimed is that the radiation detector comprising a radiation sensitive element and the load, with the sensitive element connected at one side to a voltage supply bus and the load being connected at one side to a common bus, additionally comprises a switching-type transistor, a capacitor and an interrogation pulse generator, with the sensitive element being connected at the other side to the first transistor electrode and the first plate of the capacitor, the second plate of which is connected to the load signal contact, and the output of interrogation pulse generator being connected to the control electrode of the transistor, the third electrode of which is

connected to the common bus. Besides, N groups of elements is connected between the supply voltage bus and the common bus, and each group comprises the series-connected radiation sensitive element and the transistor, the common point of which is coupled with the load signal contact though the capacitor, and the interrogation pulse generator comprises N outputs, each being connected to the transistor control electrode from the respective group of elements, where  $N - \text{integer} > 1$ .

Additionally, the detector may comprise L loads, with the signal contact of each i-th load being connected to  $N_i$  groups of elements, and the total number of groups of elements in the detector equals the N number of interrogation pulse generator outputs, where  $L - \text{integer} > 1$ , and  $N_i - \text{positive integer}$ . In addition, a resistor is connected between the sensitive element and the common point of the switching-type transistor and capacitor.

[0005] The subject-matter of the third embodiment of the invention being claimed is that the radiation detector comprising a radiation sensitive element and a load, with the sensitive element being connected at one side to a supply voltage bus and the load being connected at one side to a common bus, additionally comprises a transistor and an interrogation pulse generator, with the sensitive element being connected at the other side to the first transistor electrode, the output of the interrogation pulse generator being connected with the control electrode of the transistor, the third electrode of

which is connected to the load signal contact. In addition, a capacitor is connected between the first transistor electrode and common bus, and a resistor is connected between the first transistor electrode and the sensitive element.

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[0006]

SUMMARY OF THE INVENTION

[0007] The object of the invention being claimed is to increase sensitivity and accuracy in detecting radiation intensity and also to expand a dynamic range of radiation intensities to be detected.

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[0008] The accuracy and sensitivity in measuring the radiation intensity in the first embodiment of the invention being claimed comprising a series-connected photodiode and a load as in prior art is increased by incorporating additionally a switching-type transistor and an interrogation pulse generator into the detector, with the respective connections of said elements to the other detector elements being provided. As a result, a photodiode photocurrent is converted from the direct photocurrent to the pulse photocurrent, which small quantity can be measured at a higher accuracy due to the fact that the current amplifies and charge pulse amplifiers do not comprise low-frequency noise components, such as flicker and zero drift, that are characteristic of dc current amplifiers. Placing N groups of elements consisting of a transistor and a photodiode coupled with N outputs of the interrogation pulse generator in parallel with the load provides a new quality to the radiation

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detector, i.e. a capability of analyzing the spatial distribution of intensity of the to-be-detected radiation. In comparison with the conventional one-dimensional photodiode strips [3] the embodiment being claimed allows for achieving a wider dynamic range of radiation intensities to be detected.

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This is conditioned by the fact that the dynamic range determined as the ratio of the maximum registered radiation intensity to the minimum one is defined by the range of an electric charge integrated at the photodiode capacitance and by the integrating period range of said charge. The range of the charge integrated at the photodiode capacitance is determined as the ratio of a maximum value of the integrated charge to the noise charge of the amplifier detecting said charge. All other factors being equal, the range of the charge integrated at the photodiode capacitance is directly proportional to the square root of the capacitance value thereof, since the maximum value of the charge integrated at the photodiode increases in direct proportion to the capacitance value thereof, whereas the value of the noise charge of the amplifier increases in direct proportion only to the square root of the capacitance value at the input thereof [5]. The period range of photocurrent integrating at the photodiode capacitance in its turn is determined by the ratio of the maximum value thereof to the minimum one. The maximum duration of the photocurrent integrating period is determined by the leakage resistance of the photodiode, transistor and circuit board insulation and

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increases directly with the increase in the total capacitance of the photodiode and switching-type transistor. The minimum duration of the photocurrent-integrating period is determined by the time constant of the total capacitance discharge of the photodiode and switching-type transistor during the process of forming of an integrated discharge readout signal. The duration of said time constant is directly proportional to the total capacitance of the photodiode and switching-type transistor and to the switch-on resistance of the switching-type transistor.

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Therefore, the larger the capacitance of the photodiode and the charge leakage resistance therefrom, as well as the lower the switch-on resistance of the switching-type transistor, the more extensive the dynamic range of radiation intensities to be detected. The embodiment being claimed is characterized in that both field-effect transistors similar to the conventional photodiode strips and bipolar transistors may be used as the detector switching-type transistors. Using bipolar transistors, the steepness of which exceeds hundreds of times that of field-effect transistors, as switching-type transistors of the detector being claimed allows the switch-on resistance of the switching-type transistor to be decreased hundreds-fold and, respectively, the dynamic range of to-be-detected radiation intensities to be expanded hundreds-fold. To produce the preset dynamic range of the radiation intensities to be detected, the capacitors of the required capacitance are placed in parallel

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with the photodiodes. To reduce the amplifier noises, the detector may contain L loads.

[0009] Increasing sensitivity and accuracy in detecting the radiation intensity in the second embodiment of the invention being claimed including a radiation-sensitive element and a load like in the prior art is attained by additionally incorporating a transistor and an interrogation pulse generator into the detector, with the respective connections of said elements to the other detector elements being provided. Connecting N groups of elements consisting of the switching-type transistor, a radiation-sensitive element and a capacitor, which are connected to the N outputs of the interrogation pulse generator, between the supply voltage bus and common bus provides a new quality to the radiation detector, i.e. a capability of analyzing the intensity spatial distribution of the radiation to be detected. The second embodiment of the detector being claimed (like the first embodiment) allows for achieving a more extensive dynamic range of radiation intensities to be detected, compared with the conventional one-dimensional photodiode strips, as well as allows for using radiation-sensitive elements such as proportional counters, ionizing chambers, photoresistors, etc. requiring high supply voltage and, as a result, expanding the range of possible detector applications. The increase in sensitivity and accuracy in detecting the radiation, as well as the expansion of the dynamic range of the radiation intensities to be detected is achieved in the second embodiment being

claimed due to the action of factors leading to attaining similar technical results in the first embodiment being claimed.

To reduce amplifier noises, the detector may contain L loads.

[0010] Increasing sensitivity and accuracy in detecting the radiation intensity in the third embodiment of the invention being claimed including a radiation-sensitive element and a load like in the prior art is attained by additionally incorporating a switching-type transistor and an interrogation pulse generator into the detector, with the respective connections of said elements to the other detector elements being provided. The increase in sensitivity and accuracy in detecting the radiation is achieved in the third embodiment being claimed due to the action of factors leading to attaining similar technical results in the first embodiment being claimed. To achieve the preset dynamic range of the radiation intensities to be detected, a capacitor of the required capacitance is connected between the first switching-type transistor electrode and common bus.

[0011] BRIEF DESCRIPTION OF THE DRAWINGS

[0012] Figs. 1, 2, 3 show three modifications of an electric circuit of the first embodiment of the radiation detector being claimed that uses photodiodes as sensitive elements.

[0013] Figs. 4, 5, 6 and 7 show four modifications of an electric circuit of the second embodiment of the radiation detector being claimed that uses different types of sensitive

elements and operates when a bias voltage, including high bias voltage, is supplied thereto.

[0014] Figs. 8 and 9 show two modifications of an electric circuit of the third embodiment of the detector being claimed that uses different types of sensitive elements operating when energized by a bias voltage.

5 [0015] DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0016] A radiation detector being provided comprises an interrogation pulse generator 1, a radiation sensitive element 2 (a photodiode in the first embodiment of the detector being provided), a switching-type transistor 3 and a load 4. In the second and third embodiments, the detector may also include a current-limiting resistor 5. In the first detector embodiment (see Figs. 1, 2, 3) the photodiode 2 and load 4 are series-connected, with the load 4 being coupled through a signal contact with the photodiode 2 and with the common bus at the other side. The second electrode of the photodiode 2 is coupled with the first electrode (for example, emitter) of the switching-type transistor 3; the control electrode (for example, base) is coupled with an output of the interrogation pulse generator 1 through a resistor 6; and the third electrode of the transistor 3 (for example, a collector) is coupled with the common bus. An integrating capacitor 7 may be placed in parallel with the photodiode 2. In the second modification of the first detector embodiment (see Fig. 2), N groups of  $8_1, 8_2, \dots, 8_N$

elements, each consisting of the series-connected switching-type transistor 3 and photodiode 2, with which the integrated capacitor 7 may be placed in parallel, is connected across the load 4. Besides, the interrogation pulse generator 1 comprises N outputs, each being connected to the control electrode (base) of the switching-type transistor 3 from the respective group of elements via resistor 6, where  $N - \text{integer} > 1$ . In the third modification of the first detector embodiment (see Fig. 3), L loads  $4_1, 4_2, \dots 4_L$  are included, with above-mentioned  $N_i$  group of elements being placed in parallel with each i-th load, and the interrogation pulse generator 1 comprising N outputs, the number of which equals the total number of groups of elements in the detector, where  $L - \text{positive integer} > 1$ , and  $N_i - \text{positive integer}$ .

[0017] In the second embodiment of the detector being provided (see Figs. 4, 5, 6, 7), another types of elements, for example, ionization chambers (see Fig. 4) or ionizing radiation proportional counters (see Fig. 5, 6, 7) may be also used in addition to photodiodes as sensitive elements 2. The first simplest modification of the second embodiment of the detector being provided (see Figs. 4, 5) includes an interrogation pulse generator 1, a radiation sensitive element 2, a switching-type transistor 3, a load 4, a current-limiting resistor 5 and an integrating capacitor 7. In this case, the radiation sensitive element 2 is coupled with the supply voltage bus at one side and, via the current limiting resistor 5, with the first

electrode (for example, a drain region or emitter) of the switching-type transistor 3 and the first plate of the integrating capacitor 7 at the other side, the second plate of the latter being connected to the signal contact of the load 4, the second contact of which is coupled with the common bus.

Besides, the output of the interrogation pulse generator 1 is coupled with the control electrode (gate or base) of the switching-type transistor 3. It should be noted, that in case a bipolar transistor serves as the switching-type transistor 3, the resistor 6 is connected between the generator 1 output and transistor 3 base (see Fig. 5). The third electrode (for example, source or collector) of the switching-type transistor 3 is coupled with the common bus. A constant voltage  $A_1$  of the required polarity and value is supplied to the supply voltage bus. Both field-effect transistors (see Fig. 4) and bipolar transistors (see Fig. 5) may be used as the switching-type transistor 3.

[0018] In the second embodiment of the detector being provided, it is most reasonable to use elements sensitive to various radiation types needing the bias voltage, including high bias voltage, to be supplied for an efficient operation. In the second modification of the second embodiment of the radiation detector being provided (see Fig. 6), N groups of  $8_1$ ,  $8_2$ , ...,  $8_N$  elements, each consisting of a series-connected radiation-sensitive element 2 and a switching-type transistor 3, the common point of which being coupled with the signal contact of

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the load 4 via the integrating capacitor 7, are connected between the supply voltage bus and common bus. Besides, the interrogation pulse generator 1 comprises N outputs, each being coupled with the control electrode (base) of the switching-type transistor 3 via the resistor 6 from the respective group of elements, where  $N - \text{integer} > 1$ . In the third modification of the second radiation detector embodiment (see Fig. 7) L loads  $4_1, 4_2, \dots 4_L$  are included with the signal output of each i-th load is connected to the above-mentioned  $N_i$  groups of elements, and the interrogation pulse generator contains N outputs, the number of which equals the total number of groups of elements in the detector, where  $L - \text{integer} > 1$  and  $N_i - \text{positive integer}$ .

In the third embodiment of the radiation detector being provided (see Figs. 8, 9), the other types of sensitive elements 2 requiring a bias voltage supply for an efficient operation, for example, for photoresistors (see Fig. 8), may be also used in addition to photodiodes. The first simplest modification of the third embodiment of the detector being provided (see Fig. 8) comprises an interrogation pulse generator 1, a radiation-sensitive element 2, a switching-type transistor 3, a load 4 and a current-limiting resistor 5. In this case, the radiation-sensitive element 2 is coupled at one side with the voltage supply bus and at the other side - with the first electrode (for example, drain) of the switching-type transistor 3 via the current-limiting resistor 5. The output of the interrogation pulse generator 1 is coupled with the control electrode (gate)

of the switching-type transistor 3, the third electrode of which (for example, source) is coupled with the signal contact of the load 4 connected to the common bus at the other side. A constant voltage  $A_1$  of the required polarity and value is delivered to the voltage supply bus. The second modification of the third radiation detector embodiment (see Fig. 9) additionally comprises an integrating capacitor 7, being connected between the first electrode (for example, drain) of the switching-type transistor 3 and common bus. Field-effect transistors, the self-capacitance of which is used as an integrating capacitance in the first modification of said detector embodiment, may be used as the switching-type transistor 3 only in the third embodiment of the radiation detector being provided.

[0019] The radiation detector provides the interrogation pulse generator 1 being a rectangular voltage-pulse generator. The amplitude and polarity of output voltage pulses are selected to enable the respective detector switching-type transistors thereby. Ring counters, decoders, shift registers and other devices having the number of outputs equaling those of switching-type transistors in the detector and forming the voltage pulses of the required polarity, amplitude and duration on outputs at the respective points of time may be used as the generator 1 in multi-element detector modifications. The generator 1 frequency sets the integrating period of the radiation recorded by the detector and defines the limit of the intensity registered.

[0020] The operation of the radiation detector is described below.

[0021] The current of the sensitive element 2, when exposed to radiation, integrates at the common capacitance of the sensitive element 2 and paralleled integrating capacitor 7 (see Figs. 1, 2, 3), at the capacitance of the integrating capacitor 7 (see Figs. 4-7), at the self-capacitance of the switching-type transistor 3 and integrating capacitor 7 (see Fig. 9) during the time between interrogations of the transistor 3. An interrogation voltage pulse with polarity activating the transistor 3 is supplied from the generator 1 output to the transistor 3 control electrode at the time the switching-type transistor 3 is being interrogated. As a result of activation of the transistor 3, a current pulse carrying a charge integrated at the capacitor 7 (as well as at the capacitance of the sensitive element 2 or at the capacitance of the transistor 3) through the capacitor 7 and load 4 flows therethrough. While supplying the interrogation pulse, interelectrode-capacitance recharging charges flow via the load 4, via the capacitance of the sensitive element 2 and/or integrating capacitor 7 (see Figs. 1-7) or directly (see Figs. 8, 9). The charges equal in value, but opposite in sign flow via said circuits upon removing the interrogation parts. As a result, after supplying each interrogation pulse, a total charge flows through the load 4 equaling the charge of said element integrated at the capacitor 7 and/or at the self-capacitance of the sensitive element 2 over

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the time interval between supplying the interrogation pulse. In  
case the load 4 is connected between the switching-type  
transistor 3 and common bus (see Fig. 8, 9), after supplying the  
interrogation pulse, the charge of the sensitive element 2  
integrated at the total capacitance of the capacitor 7 and/or  
transistor 3 is carried to the load 4. Said charge is  
proportional to a radiant flux incident on the sensitive element  
2 over the time interval between interrogations of the  
respective switching-type transistor 3.

[0022] In multi-element modifications of the detector (see  
Figs. 2, 3, 6, 6), the interrogation pulse generator 1 is  
provided with a plurality of outputs, with voltage pulses  
forming on each of them in a preset sequence. In this case, a  
serial interrogation of switching-type transistors 3, which are  
included into the groups of elements 8, corresponding, for  
example, to a sequential reading out of the respective  
integrating capacitors 7, is performed, while a sequence of  
current pulses, displayed as video signals, form at the load 4,  
when synchronizing clock is added thereto at the respective  
instant of time. It should be noted that the coordinate of the  
detector sensitive element is uniquely defined by the number of  
the load pulse corresponding thereto or by the time said pulse  
is generated, while the number of radiation particles detected  
in said sensitive element is defined by the amplitude of the  
current pulse corresponding thereto. In the detector  
modifications having plurality of loads (see Figs. 3, 7), the

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sequence of interrogation current pulses forms serially at each load at time intervals of interrogation of switching-type transistors incorporated into the groups of elements 8 coupled with said load. Availability of a plurality of loads in the detector allows the total number of sensitive elements to be increased in the detector without increasing the noise of amplifier integrating capacitors detecting the readout signals. In addition to the increased radiation detection sensitivity, the capability of the detector being provided to analyze space-energy characteristics of various types of radiation fields to be detected within an extensive intensity range significantly expands functional capacities and application field thereof. The invention may be used in the fields of nuclear physics, dosimetry, radiation flaw inspection, photometry, crystallography, medicine and other fields of science and engineering.

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